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(REV 3/2001)

U.S. DEPARTMENT OF COMMERCE PATENT AND TRADEMARK OFFICE

DATE: December 18, 2001

EXPRESS MAIL LABEL NO.
EL 914619345 USATTORNEY DOCKET NO.
33683/TJD/T358

U.S. APPLICATION NO.

To Be Assigned
10/018923TRANSMITTAL LETTER TO THE UNITED STATES
DESIGNATED/ELECTED OFFICE (DO/EO/US)
CONCERNING A FILING UNDER 35 U.S.C. 371INTERNATIONAL APPLICATION NO
PCT/US 99/13934INTERNATIONAL FILING DATE
22 June 1999PRIORITY DATE CLAIMED
22 June 1999

TITLE OF INVENTION

BACK-FLUSHING SPIRAL WOUND FILTER AND METHODS OF MAKING AND USING SAME

APPLICANT(S) FOR DO/EO/US

Peter H. Knappe et al.

Applicant herewith submits to the United States Designated/Elected Office (DO/EO/US) the following items and other information:

1. ☒ This is a **FIRST** submission of items concerning a filing under 35 U.S.C. 371.
2. ☐ This is a **SECOND** or **SUBSEQUENT** submission of items concerning a filing under 35 U.S.C. 371.
3. ☒ This is an express request to begin national examination procedures (35 U.S.C. 371(f) at any time rather than delay examination until the expiration of the applicable time limit set in 35 U.S.C. 371(b) and PCT Articles 22 and 39(1).
4. ☒ A proper Demand for International Preliminary Examination was made by the 19th month from the earliest claimed priority date.
5. ☒ A copy of the International Application as filed (35 U.S.C. 371(c)(2)).
 - a. ☐ is transmitted herewith (required only if not transmitted by the International Bureau).
 - b. ☐ has been transmitted by the International Bureau.
 - c. ☒ is not required, as the application was filed in the United States Receiving Office (RO/LUS).
6. ☐ A translation of the International Application into English (35 U.S.C. 371(c)(2)).
7. ☒ A copy of the International Search Report (PCT/ISA/210)
8. ☒ Amendments to the claims of the International Application under PCT Article 19 (35 U.S.C. 371(c)(3)).
 - a. ☐ are transmitted herewith (required only if not transmitted by the International Bureau).
 - b. ☒ have been transmitted by the International Bureau.
 - c. ☐ have not been made; however, the time limit for making such amendments has NOT expired.
 - d. ☐ have not been made and will not be made.
9. ☐ A translation of the amendments to the claims under PCT Article 19 (35 U.S.C. 371(c)(3)).
10. ☒ An oath or declaration of the inventor(s) (35 U.S.C. 371(c)(4)).
11. ☒ A copy of the International Preliminary Examination Report (PCT/IPEA/409).
12. ☐ A translation of the annexes to the International Preliminary Examination Report under PCT Article 36 (35 U.S.C. 371(c)(5)).

Items 13 to 20 below concern document(s) or other information included:

13. ☐ An Information Disclosure Statement under 37 CFR 1.97 and 1.98.
14. ☐ An assignment document for recording. A separate cover sheet in compliance with 37 CFR 3.28 and 3.31 is included.
15. ☒ A **FIRST** preliminary amendment.
16. ☐ A **SECOND** or **SUBSEQUENT** preliminary amendment.
17. ☐ A substitute specification.
18. ☐ A change of power of attorney and/or address letter.
19. ☒ **SMALL ENTITY** Assertion: Applicant(s) and any other associated with it/them under 37 CFR § 1.27(a) are a small entity.
20. ☒ Certificate of Mailing by Express Mail.
21. ☐ Other items or information:

U.S. APPLICATION NO. 10/018923 (If known, see 37 CFR 1.5)		INTERNATIONAL APPLICATION NO. PCT/US 99/13934		ATTORNEY DOCKET NO. 33683/TJD	
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21. The following fees are submitted:				CALCULATIONS	PTO USE ONLY
<input type="checkbox"/>	Neither international preliminary examination fee (37 CFR 1.482) nor international search fee (37 CFR 1.445(a)(2)) paid to USPTO and International Search Report not prepared by the EPO or JPO.		\$1,040.00		
<input type="checkbox"/>	International preliminary examination fee (37 CFR 1.482) not paid to USPTO but International Search Report prepared by the EPO or JPO		\$890.00		
<input type="checkbox"/>	International preliminary examination fee (37 CFR 1.482) not paid to USPTO but international search fee (37 CFR 1.445(a)(2)) paid to USPTO		\$740.00		
<input checked="" type="checkbox"/>	International preliminary examination fee paid to USPTO (37 CFR 1.482) but all claims did not satisfy provisions of PCT Article 33(1)-(4)		\$710.00		
<input type="checkbox"/>	International preliminary examination fee paid to USPTO (37 CFR 1.482) and all claims satisfied provisions of PCT Article 33(1)-(4)		\$100.00		
ENTER APPROPRIATE BASIC FEE AMOUNT =				\$ 710.00	
Surcharge of \$130 for furnishing the oath or declaration later than <input type="checkbox"/> 20 <input checked="" type="checkbox"/> 30 months from the earliest claimed priority date (37 CFR 1.492(e)).				\$ 130.00	
Claims	Number Filed	Number Extra	Rate		
Total Claims	65 -20=	45	X \$18	\$ 810.00	
Independent Claims	9 -3=	6	X \$84	\$ 504.00	
Multiple dependent claim(s) (if applicable)			+ \$280	\$	
TOTAL OF ABOVE CALCULATIONS =				\$2,154.00	
Reduction by 1/2 for filing by small entity, if applicable. Verified Small entity statement must also be filed. (Note 37 CFR 1.9, 1.27, 1.28).				\$1,077.00	
SUBTOTAL =				\$1,077.00	
Processing fee of \$130 for furnishing the English translation later than <input type="checkbox"/> 20 <input type="checkbox"/> 30 months from the earliest claimed priority date (37 CFR 1.492(f)).				\$ —	
TOTAL NATIONAL FEE =				\$1,077.00	
Fee for recording the enclosed assignment (37 CFR 1.21(h)). The assignment must be accompanied by an appropriate cover sheet (37 CFR 3.28, 3.31). \$40.00 per property				\$ —	
TOTAL FEES ENCLOSED =				\$1,077.00	
Note (1): The basic national fee must be paid when filing this application. The 20-month time limit (37 CFR § 1.494) and 30-month time limit (37 CFR § 1.495) are not extendable.				Amount to be:	
				refunded	\$
				charged	\$

a. ☒ A check in the amount of **\$ 1,077.00** to cover the above fees is enclosed.

b. ☐ Please charge my Deposit Account No. _____ in the amount of \$ _____ to cover the above fees.
A duplicate copy of this sheet is enclosed.

c. ☒ The Commissioner is hereby authorized to charge any additional fees which may be required, or credit any overpayment to Deposit Account No. **03-1728**. A duplicate copy of this sheet is enclosed.

NOTE (2): Where an appropriate time limit under 37 CFR 1.494 or 1.495 has not been met, a petition to revive (37 CFR 1.137(a) or (b)) must be filed and granted to restore the application to pending status.

SEND ALL CORRESPONDENCE TO:

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10/018923

531 Rec'd PC

19 DEC 2001
PATENT

IN THE UNITED STATES PATENT AND TRADEMARK OFFICE

EXPRESS MAIL NO. EL 914619345US

Applicant : Peter H. Knappe et al.
Application No. : To be assigned
Filed : December 18, 2001
Title : BACK-FLUSHABLE SPIRAL WOUND FILTER
AND METHODS OF MAKING AND USING
SAME
Docket No. : 33683/TJD/T358

PRELIMINARY AMENDMENT

Assistant Commissioner for Patents
Washington, D.C. 20231
Commissioner:

Post Office Box 7068
Pasadena, CA 91109-7068
December 18, 2001

Please amend the above-identified patent application as follows:

In the Specification:

Page 1, line 4, insert:

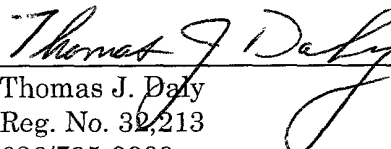
CROSS-REFERENCE TO RELATED APPLICATIONS

This application claims the priority to PCT Patent Application
No. PCT/US99/13934, filed on June 22, 1999.

Respectfully submitted,

CHRISTIE, PARKER & HALE, LLP

By


Thomas J. Daly
Reg. No. 32,213
626/795-9900

TJD/sad
SAD PAS400016.1-*12/17/01 4:19 PM

1

BACK-FLUSHABLE SPIRAL WOUND FILTER AND
METHODS OF MAKING AND USING SAME

BACKGROUND OF THE INVENTION

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Membrane fouling is generally recognized as the outstanding problem in modern membrane separations. A full discussion of the problems, specifically associated with ultrafiltration, can be found in "Fifteen Years of Ultrafiltration" by Micheals, A.S. in Ultrafiltration Membranes and Applications edited by A.R. Cooper (American Chemical Society Symposium, Washington, 9-14 Sept. 1979, Plenum Press, New York (1980); ISBN 0-306-40548-2) where it is stated that "the problems of reduced throughput, capacity, increased power consumption, compromised separation capability, and reduced membrane service lifetime associated with macro-, solute- and colloid-fouling of ultrafiltration membranes have stubbornly resisted adequate solution despite ten years of engineering experience in pilot and full-scale industrial situations."

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According to Micheals, back-flushing by reverse flow of permeate in hollow-fiber membrane modules, significantly aids in unplugging of membrane pores and detachment of adhering deposits. However, there are only two specific examples of permeate back-flushing described in that text and these concern filtration of tap water and of electro-deposition paints emulsified in water.

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As set forth at pages 109 to 227 of the above text, back-flushing of hollow fibers with permeate is used where operating transmembrane pressures are only about one atmosphere so that particles are not driven hard into membrane pores during the filtering process. As indicated above, permeate back-flushing has been used where the fouling species are in liquid paint emulsion droplets as these species do not wedge into the membrane pores as do solids. As the transmembrane flux is often only five to twenty liters per square meter per hour (L/m^2 hr), the corresponding fluid velocity is only a few millimeters per hour and there is, therefore, no possibility of a high velocity cleaning action.

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Permeate back-flushing is, in essence, a recycling process and, thus, a sacrifice of production rate is only justified when the cleaning effect is significant. Some sticky natural wastes (such as brewing residues, starch, and egg) are not removed to any appreciable extent by permeate back-flushing. According to Micheals, permeate back-flushing is, by definition, a purely hydraulic flow through totally wetted pores of the ultrafiltration membrane.

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In U.S. Patent No. 4,767,539, Ford describes an improved method of back-flushing hollow fiber filters which uses a gas back-flush medium. Ford's invention uses the back-flush gas at a pressure of about 500 kilopascals to swell the fiber from the inside and erupt around the elastic openings. This gas back-flush resulted in better removal of foulants from the surface of the membrane than did the standard permeate back-flush. The penetration of gas into the pores of a membrane is resisted by the surface tension forces of the contained wall-wetting liquid. Indeed,

1 surface tension is conveniently measured by the breakthrough pressure needed to force a bubble
out of a submerged orifice. For common systems (such as oil in hydrophobic pores or water in
hydrophilic pores) the breakthrough pressure required ranges from ten kilopascals to a thousand
kilopascals. The breakthrough pressures are much higher than the usual operating pressures of
5 the filter.

In U.S. Patent No. 5,248,424, Cote describes a frame-less array of hollow fiber
membranes and a method of maintaining a clean fiber surface while filtering a substrate and
withdrawing permeate. A scrubbing gas is used to sway the free floating fibers and thus
minimizes or eliminates the build-up of foulants and biological organisms on the membrane
10 surface.

Historically, difficult feed solutions with high organic and suspended solids have been
treated with capillary (0.3 – 1.0 mm dia) or tubular element designs. While these designs are
effective, they have a number of limitations, notably, the materials of construction must be
chosen not just for the permeability and rejection characteristics needed to perform separations,
but also for mechanical strength to withstand the feed pressures required for operation, including
back-flush. The hollow fiber and tubular constructions also have relatively low packing densities
of active membrane area, thus the cost per unit area is high.

All of the above-mentioned devices are manufactured in a hollow fiber configuration.
While this design has many advantages, it is not as versatile and cost effective as spiral wound
membrane designs. Spiral wound membrane filtration elements with microfiltration (MF),
ultrafiltration (UF), nanofiltration (NF), and reverse osmosis (RO) membranes, are used for
treating drinking or process water that is relatively low in suspended solids and organic foulants.

Increasingly, more and more difficult feed solutions are being treated with spiral wound
elements. Spiral wound elements have several advantages over hollow fiber and tubular
elements. The membranes are cast on a woven or non-woven support substrate which lends
structural strength and allows easy membrane formation. Support fabric substrates allow
membranes to be formed as composites, with the base membrane providing a strong and defect
free support surface over which can be coated a thin barrier layer that dictates the transport
properties. Also, the spiral wound configuration has a high packing density, has a low production
25 cost, is easily scaled up to large systems, and replacement is easy and inexpensive. In most
current commercial applications using UF, NF, or RO where spiral elements can operate
effectively, they have become the design of choice due to the above mentioned benefits.

However, most spiral wound elements can not be back-flushed due to failure of the
adhesive seals and delamination of the membrane film from the support fabric substrate. A recent
35 survey of warranty literature from manufacturers of the large majority of spiral wound element
filters all contain strong, unequivocal language reaffirming that any back pressure would damage
the elements and are conclusive grounds for voiding the membrane element warranty. A design
for spiral wound elements that would allow for effective back-flushing is needed.

SUMMARY OF THE INVENTION

It is an object of this invention to provide a spiral wound membrane and element configuration capable of being back-flushed, and an improved method of processing and back-flushing fluids using spiral wound membrane elements.

A spiral wound membrane filtration element capable of being back-flushed has a permeate carrier sheet, a membrane filter layer sheet adhesively bonded to the permeate carrier sheet, and a feed spacer sheet in between layers of membrane filter layer sheets. The membrane filter layer sheet is normally folded in half, over a feed spacer sheet. An active membrane film side of the membrane filter layer sheet faces both sides of the feed spacer. The feed spacer sheet, the membrane filter layer sheets, and the permeate carrier sheet are wrapped around a permeate collection tube.

The membrane filter layer sheet further has a support substrate with a Frazier air permeability between 1 and 10 cfm/ft². The membrane filter layer sheet may be homogenous or asymmetric. For a homogenous membrane filter layer sheet, polymeric film may be encased around a support substrate or be a self-supporting polymeric film. In an asymmetric membrane filter layer sheet, the polymer film is cast on top of a support substrate, and adequately bonded thereto in order to eliminate delamination during a back-flush cycle.

The permeate carrier fabric sheet acts as a conduit that allows the part of the feed solution which permeates the membrane filter layer sheet to exit the element via the permeate collection tube which is in the center of the element. Each membrane filter layer sheet is bonded to the permeate carrier fabric sheet on the three sides not adjacent to the permeate collection tube with an adhesive capable of retaining the seal throughout a back-flushing of the element.

A method of making a back-flushable spiral wound membrane filtration element comprises forming a membrane filter layer sheet, cutting the membrane filter layer sheet to a desired length, placing a cut piece of a feed spacer sheet on top of the membrane filter layer sheet, the width of the feed spacer sheet being approximately half the width of the membrane filter layer sheet; folding the membrane filter layer sheet over the feed spacer so that the feed spacer sheet is sandwiched between two layers of the membrane filter layer sheet; attaching a center side part of a permeate carrier sheet to the permeate collection tube; applying an adhesive seal on the permeate carrier sheet along sides other than the center side part; positioning the membrane filter layer sheet-feed spacer sheet sandwich over the permeate carrier sheet such that the adhesive seal bonds the membrane filter layer sheet to the permeate carrier sheet; and wrapping the permeate carrier sheet, the membrane filter layer sheet, and the feed spacer sheet around the permeate collection tube.

A method of creating a permeable membrane filter layer sheet comprising placing a casting solution of a certain thickness on a passing support substrate; controlling the thickness of the casting solution on the support substrate through use of a mechanical device for dispensing the casting solution; and immersing the substrate with the casting solution into a quench bath to

1 allow removal of casting solution after an air quench time that allows formation of a thin skin on the support substrate.

5 A preferred back-flush system for the back-flushable spiral wound membrane filtration element comprises a feed solution for the filtration element from a source; a pump suction pipe having a shut off valve, the pump suction pipe used in withdrawal of the feed solution; a feed pump for pumping and pressurizing the feed solution from the source through the filtration element; a feed valve for controlling the pump discharge pressure; a feed pressure gauge for measuring the feed pressure from the pump; a feed pipe through which the pressurized feed solution flows to the element; an element pressure tube wherein a first portion of the feed
10 solution permeates the membrane filtration element as a permeate, and a second portion of the feed solution does not permeate and exits the membrane filtration element as a concentrate; a feed diverter valve for controlling flow from the feed pipe to the pressure tube; a gas tank having a gas regulator and compressed gas capable of back-flushing the membrane filtration element; a concentrate diverter valve for controlling the flow rate of concentrate out of the exiting pressure
15 tube; a concentrate valve for controlling the flow rate of concentrate out of the concentrate diverter valve; a concentrate flow meter for measuring the concentrate flow out of the concentrate valve; a permeate accumulator capable of holding permeate for the back-flush step; a permeate diverter valve for controlling the flow rate of permeate out of the permeate accumulator and for controlling the flow rate of gas out of the tank while back-flushing; and a permeate flow meter for measuring permeate flow out of the permeate diverter valve.
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25 Another preferred method of back-flushing the spiral wound membrane filtration element through the back-flush system comprises gathering feed solution for the filtration element from a source; withdrawing feed solution from the source through a pump suction pipe having a shut off valve; pumping the feed solution from the source using a feed pump; pressurizing the feed solution in the pump; pumping the pressurized feed solution through the filtration element using the feed pump; controlling the pump discharge pressure using a feed valve; measuring the feed pressure from the pump using a feed pressure gauge; controlling flow from a feed pipe to the element using a feed diverter valve; permeating the membrane filtration element with a portion of the feed solution as a permeate; allowing a second portion of the feed solution which does not
30 permeate the membrane filtration element to pass through the membrane filtration element as a concentrate; pressurizing back flush fluid in a gas tank used for back-flushing the membrane filtration element; controlling the flow rate of concentrate out of the element using a concentrate diverter valve; controlling the flow rate of concentrate out of the concentrate diverter valve using a concentrate valve; measuring the concentrate flow out of the concentrate valve using a concentrate flow meter; holding permeate for the back-flush step using a permeate accumulator;
35 controlling the flow rate of permeate out of the permeate accumulator and the flow rate of gas out of the tank while back-flushing using a permeate diverter valve; measuring permeate flow out of the permeate diverter valve using a permeate flow meter; and cleaning the spiral wound

1 membrane filtration element having a membrane with pores through back-flushing the element.

Methods of cleaning a spiral wound membrane filtration element and system useful for filtering feed solution are carried out by pressurizing the feed solution or by creating a vacuum in the permeate collection tube, and periodically introducing a pressurized back flush fluid into the permeate collection tube of the filtration element to back-flush the membrane, under a pressure and for a time sufficient to dislodge a substantial portion of the retained solids on the surface of the membrane.

BRIEF DESCRIPTION OF THE DRAWINGS

10 FIG. 1 shows a spiral wound element back-flush system employing a single element pressure tube mounted in a vertical position;

FIG. 2 shows a cross-sectional view of multiple filters in an element pressure tube;

FIG. 3 shows the relationship of permeate flux versus time operating sequence for a back-flushed element system according to one embodiment of the invention;

FIG. 4 shows a perspective view of how a membrane filter layer sheet, a permeate carrier fabric sheet, and a feed spacer sheet are arranged around a permeate collection tube;

FIG. 5 shows a side view of a process system wherein the membrane film is cast onto a support substrate; and

FIG. 6 shows another embodiment of the back-flush system using an element submersed vertically in a tank with a vacuum being applied as the driving force to remove permeate.

DETAILED DESCRIPTION OF THE PREFERRED EMBODIMENTS

A first preferred embodiment of the present invention is shown in FIG. 1. A spiral element back-flush system 1 has a feed tank 2, a feed pump 6, an element pressure tube 7, and a compressed gas tank 20. Element pressure tube 7 is preferably mounted in a vertical position. Feed tank 2 contains a feed solution 100. Feed tank 2 can be replaced by a pipe from a process stream in practical applications. In this embodiment, an electric mixer 3 is shown that is used to keep the feed tank well mixed. Mixer 3 may or may not be required for commercial applications depending on the feed solution. Feed solution 100 is withdrawn from tank 2 via a pump suction pipe 4 to feed pump 6. Feed pump 6 pumps feed solution 100 through element pressure tube 7 via a feed pipe 13.

Feed solution 100 then enters element pressure tube 7 where a portion of feed solution 100 permeates a membrane filter element 15, which portion then exits pressure tube 7 to a holding tank or process stream 25 via a permeate pipe 16. The portion of feed solution 100 that permeates element 15 is permeate 101. The portion of feed solution 100 that does not pass through membrane filter element 15 is a concentrate (or brine solution) 102. Concentrate 102 that exits pressure tube 7 is directed to a holding tank or via concentrate pipe 26 back to feed tank 2 to be recycled back through filter 15.

1 Preferably, pump suction pipe 4 contains a shut off valve 5 that can be used to isolate
pump 6 for maintenance purposes. During normal operation, the pressurized feed solution from
feed pump 6 is pumped to element pressure tube 7 through a feed diverter valve 14. The flow
rate to pressure tube 7 can be controlled with a feed valve 8 and a concentrate valve 9. A feed
5 pressure gauge 12 along feed pipe 13 is used to measure the feed pressure from pump 6.

Concentrate 102 is removed from the top of element pressure tube 7. Along concentrate
pipe 26, concentrate 102 passes through a concentrate diverter valve 19, concentrate valve 9, and
a concentrate flow meter 10. Concentrate flow meter 10 is used to measure the concentrate flow
from pressure tube 7 via concentrate pipe 26.

10 Permeate 101 can be removed from either the top or the bottom of pressure tube 7. Along
permeate pipe 16, permeate 101 passes through a permeate accumulator 17, a permeate diverter
valve 18, and a permeate flow meter 11. Permeate flow meter 11 is used to measure the permeate
flow from pressure tube 7 via permeate pipe 16.

During a back-flush cycle, gas is released from compressed gas tank 20 as a back-flush
15 fluid via both a pipe 21 and permeate pipe 16 to enter pressure tube 7. Upon exiting gas tank 20,
the gas passes through a gas regulator 22, pipe 21, through permeate diverter valve 18, permeate
pipe 16, permeate accumulator 17, into pressure tube 7, and eventually into a concentrate blow
down line 23. The pressure on the back-flush gas in this embodiment needs to be greater than
the feed pressure on element 15 by about 10-30 psi, which in this embodiment is controlled by
gas regulator 22. The back flush pressure range is 5 to 100 psi. Preferably, the range is between
20 and 60 psi.

Optionally, during the back-flush cycle, permeate 101 (or another back flush fluid such
as compressed fluid, compressed nitrogen, compressed air and/or cleaning solution) can be
redirected via feed diverter valve 14 and concentrate diverter valve 19 into the top of the pressure
25 tube 7, out the bottom thereof, and into concentrate blow down line 23. Concentrate blow down
line 23 could be directed into a waste holding tank or to a drain 24. The purpose of changing the
flow from a bottom up to a top down configuration is to aid in removing suspended particles
which have built up on the surface of membrane filter element 15 in pressure tube 7.

In a practical system design, several filters would be placed in series such that
30 concentrate 102 from a first filter would become the feed to a next filter (See FIG. 2). In Figure
2, one element with two filters is shown, but the element can optionally accommodate more than
2 filters.

A back-flush fluid can be a liquid or gas or a combination of both, including air, nitrogen,
helium, other non-hazardous gasses, water, detergent, and cleaning solutions. The back-flush
35 fluid is used to reverse the permeate flow. Back-flush gas can be supplied by means of a
compressor. Using the combination of a liquid and a gas back-flush, has a beneficial effect on
the cleaning action of the back-flush cycle. In this first embodiment, the combination is utilized,
such that the permeate and nitrogen are used to drive permeate back-flush system 1. The gas

1 released from compressed gas tank 20 pushes permeate 101 from permeate accumulator 17 back into element 15. Accumulator 17 retains a certain volume of permeate 101 which is used as the initial back-flush fluid, which is replaced by the nitrogen back-flush fluid when depleted.

5 FIG. 3 is a diagram illustrating the permeate flux of a membrane filter layer sheet 71 versus time. The initial permeate flux would start at a value A, and decrease with time due to membrane fouling to value B. After this operating cycle, the back-flush cycle would decrease the permeate flux very quickly to zero as indicated by value C, and then the back-flush cycle reverses the permeate flow to value D. The back-flush continues for a specified time period to value E when foulants have been removed from membrane filter layer sheet 71. Then, the back-flush pressure would be stopped which would again decrease the permeate flux to zero as indicated by value F. After a time, indicated by value G, the system would then be started up in the normal forward operation as indicated by value H, and the cycle would continue. More permeate is created than is needed to back flush the system.

15 The normal feed configuration would occur for a set period of time that is dependent on the feed supply, turbidity of the water, membrane type and flux, and other variables associated with the membrane systems. After this time period has elapsed, the back-flush cycle would be started which would run for a much shorter time period. The back flush cycle occurs at predetermined intervals that are dependent on the membrane filter layer sheet 71, element 15, feed solution 100, and operating conditions. The duration of the back-flush cycle is normally 1 to 30 seconds. To optimize the permeate output from element 15, the back-flush part of the cycle has a cycle duration of between 1 and 30 seconds, but preferably has a 5 to 15 second duration.

20 In the preferred embodiment shown in FIG. 4, the spiral wound membrane filter element 15 capable of being back-flushed comprises a minimum of three layers: a membrane filter layer sheet 71, a feed spacer sheet 70, and a permeate carrier fabric sheet 72. Membrane filter layer sheet 71 may be homogenous or asymmetric. For a homogenous membrane filter layer sheet, polymeric film may be encased around a support substrate (support fabric) or be a self-supporting polymeric film. In an asymmetric membrane filter layer sheet, the polymer film is cast on top of a support substrate. Preferably, each membrane filter layer sheet has a support substrate (support fabric) and a polymeric membrane film. The support substrate has a low resistance to fluid flow but imparts sufficient mechanical strength to the polymeric membrane film such that the polymeric membrane film does not delaminate from the substrate during the back-flushing cycle. The methods of making the membrane filter layer sheet that remains laminated during back-flushing are discussed in detail with reference to FIG. 5.

25 30 35 Membrane filter layer sheet 71 is normally folded in half, over a feed spacer sheet 70. An active membrane film side 75 of membrane filter layer sheet 71 faces both sides of feed spacer sheet 70. The third layer is permeate carrier fabric sheet 72 which acts as a conduit that allows that part of the feed solution which permeates the membrane filter layer sheet to exit the membrane filter element via a permeate collection tube 73 which is in the center of element 15.

1 Each membrane filter layer sheet 71 is bonded to permeate carrier fabric sheet 72 with an
adhesive capable of retaining the seal throughout back-flushing of the element. The seal
between the membrane filter layer sheet and the permeate carrier fabric sheet is made on the three
5 sides that are not adjacent to permeate collection tube 73, such that a center side part of permeate
carrier sheet 72 corresponds with permeate collection tube 73. The layers are then wrapped up
around permeate collection tube 73 to form the spiral wound element.

When all three layers are rolled up, each permeate carrier fabric sheet 72 is sandwiched
between the back of membrane filter layer sheet 71 to form an envelope for the permeated water.
The feed spacer sheet can have a thickness in the range of 0.02" to 0.10," but preferably is 0.04"
10 to 0.06" thick. The feed spacer sheet is sandwiched by membrane filter layer sheet 71 with the
active membrane film side 75 facing both sides of feed spacer sheet 70. The adhesive seal that
is placed around permeate carrier fabric sheet 72 allows the permeated water to flow into
permeate collection tube 73 while preventing the feed solution from entering permeate carrier
fabric sheet 72 without first permeating active membrane film side 75 of membrane filter layer
15 sheet 71. The feed spacer sheet is held in place by friction. The layers are wrapped so tightly
around the collection tube that the feed spacer sheet is not able to move.

To back flush the element, permeate that has collected in permeate accumulator 17 and/or
the gas from tank 20 is pushed back through permeate collection tube 73 and into the filter layers
of element 15. The back-flush fluid is forced into permeate carrier fabric sheet 72. Back-flush
fluid then moves back through membrane film side 75 of membrane filter layer sheet 71 to
20 dislodge any sticking particles. The fluid then travels through feed spacer sheet 70 and out the
bottom of pressure tube 7.

The driving pressure for these operations, which is normally present as a pressurized feed
solution 100 but could also be applied as a vacuum on permeate stream 101, must overcome the
25 pressure drop through feed spacer sheet 70, and in addition, once a portion of feed solution 100
permeates the membrane filter layer sheet, it also must overcome the pressure drop through
permeate carrier fabric sheet 72. Element 15 shown in FIG. 4 is the simplest element
configuration. To create elements with larger capacities, multiple leaves must be used to
minimize the pressure drop of permeate solution 101 through permeate carrier fabric sheet 72.

30 Besides delamination of membrane film 75 from support substrate 76, another area where
the spiral wound elements of the prior art would fail when exposed to back-flush pressures, is
at the membrane adhesive seal. This problem is especially true when trying to bond the permeate
carrier fabric sheet to wet membrane filter layer sheets, because it is difficult for most
polyurethane adhesives to penetrate into a saturated substrate without the isocyanate functional
35 group reacting with the water. It is important to note that the feed pressure is actually
compressing the adhesive seal in normal operation and thus there is normally not a requirement
for the adhesive seal to have good peel strength, only that it not allow any feed solution to bypass
into the permeate collection tube.

1 To obviate the problem of lack of adhesion during back-flushing operation of spiral wound
element filters, an adhesive has been manufactured by E.V. Roberts of Culver City, California,
model number 1752. The adhesive was custom formulated to our performance specifications.
The adhesive is such that, during the back flush cycle where the seals are tensioned rather than
5 compressed, membrane filter layer sheets 71 remain sealed to permeate carrier fabric sheet 72.
This adhesive gives superior penetration and peel strength, even when membrane filter layer
sheet 71 is in a wet condition, such that delamination under back-flush conditions is prevented.

The characteristics of the adhesive include being a two-part polyurethane adhesive, being
thixotropic, having a high viscosity, having good penetration into the support substrate, not being
10 too sensitive to moisture (in that it can be applied to wet membrane filter layer sheets and still
retain it's bonding properties), and being thick enough to coat the permeate carrier fabric sheet
so as not to leave gaps. The specifications of the adhesive vary depending on whether the
finished membrane layer sheet is dry or wet. For example, urethanes are very reactive with
water. The reaction with the urethanes will form a gas thereby leaving voids in the adhesive line.
15 Using different isocyanate groups for wet membrane layer sheets will not form this gas.

Generally, the preferred two-part polyurethane adhesive includes an "A" component and
a "B" component that are shipped in separate containers. When the components are mixed
together in the proper ratios, these "two-parts" react with each other forming a cross-linked
adhesive that gels in about an hour and obtains working strength in about 6 to 8 hours. In an
20 exemplary embodiment, the adhesive is mixed in a ratio of 100 parts by weight of "A" to 173
parts by weight of "B". The work life at 25°C is about 30 to 35 minutes. The mixed viscosity
of the adhesive at 25°C is about 50,000 cps. Preferably, after 254 hours of cure, the adhesive has
a Shore A hardness of between 75 and 85 and an overlap shear strength on aluminum of between
800 and 1200, preferably at least 1000 psi, and an overlap shear strength on PVC of between 300
25 and 500, preferably at least 400 psi. These properties ensure that the adhesive retains the bond
during back flushing.

The method of making the back-flushable spiral wound membrane element comprises the
steps of forming the membrane filter layer sheet, cutting the membrane filter layer sheet to the
desired length and placing a cut piece of the feed spacer sheet on top of the membrane filter layer
30 sheet and to one side thereof. The width of the feed spacer sheet is approximately half the width
of the membrane filter layer sheet. The membrane filter layer sheet is folded over the feed spacer
so that the feed spacer sheet is sandwiched between two layers of the membrane filter layer sheet.
The permeate carrier fabric sheet is then attached to the permeate collection tube via a double
sided tape or other suitable means, and an adhesive seal is applied on the permeate carrier fabric
35 at end farthest from the permeate collection tube and at the two sides thereof. The membrane
filter layer sheet-feed spacer sheet sandwich is then positioned over the permeate carrier fabric
sheet such that the adhesive seal bonds the membrane filter layer sheet to the permeate carrier
fabric sheet. The layers are then wound around the permeate collection tube to form spiral

1 wound membrane filtration element 15.

There are several ways to create the membrane filter layer sheet having membrane film 75 and support substrate 76. See FIG. 5. Polymers that are used to create the membrane film may be dissolved in solvents or applied as melted-homogenous films. The most common method
5 for making the membrane filter layer sheet involves coating a polymer dissolved in a suitable solvent, such as dimethylformamide, 1,4 dioxane, acetone, or n-methyl pyrrolidone, onto a support substrate.

Membrane filter layer sheets that can withstand repeated cycles of back flushing must be created for either homogenous, or asymmetric designs. If the membrane film is cast where the support substrate is encased in the polymer matrix (homogeneous), a membrane filter layer sheet with excellent resistance to back-flushing is created. In the preferred embodiment, the membrane film is cast on top of the support substrate to form an asymmetric membrane filter layer sheet. For the asymmetric sheet, a sufficient bond must be created between the membrane film and the support substrate. FIG. 5 illustrates the process system wherein the membrane film is cast onto the support substrate as in the homogeneous or asymmetric membrane filter layer sheet. The homogeneous membrane filter layer sheet has a greater strength than the asymmetric sheet because the support substrate is encased in the polymer matrix, rather than polymer cast on top of the substrate. However, the processes in which homogeneous membrane filter layer sheets are used are limited. For example, the homogeneous membrane filter layer sheets function optimally with microfiltration and ultrafiltration processes.
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A homogenous membrane is formed by coating a polymeric casting solution onto a support substrate, whereby the porosity of the support and the penetration of the casting solution allows the casting solution to completely penetrate the support fabric, thereby encapsulating the support fabric inside the membrane polymer. The coated membrane film is then allowed an amount of time to form a skin, before quenching the film in a fluid bath, preferably water. The initial solvent on the outside of the sheet is rapidly removed upon insertion into the bath. Leaving the sheet in the quench bath for a time allows the remainder of the solvent, that has not diffused out of the membrane, to be removed from the membrane layer sheet. Because of the chemistry of the casting solution, and the formation of the membrane skin, the finished membrane has a surface layer with small and uniform pores. This structure is homogeneous throughout the membrane structure, thus creating a higher resistance to fluid flow and requiring a greater pressure drop than a corresponding asymmetric membrane. Upon examination of this membrane layer sheet under a scanning electron microscope (SEM), it can be seen that the pore size at the membrane surface is small and uniform, and this structure is fairly uniform throughout the membrane cross section. This symmetry, or homogeneity, is where these membranes derive their name of homogenous membranes. The porosity of the support substrate is between 0.1 and 3 cfm/ft², preferably between 0.5 and 1 cfm/ft², with a thickness of between 0.001" and 0.005", preferably between 0.002" and 0.004", and a weight between 20 and 100 gm/yd², preferably
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1 between 40 and 80 gm/yd². The chemistry and physical properties of the casting solution are
also important. The viscosity of the casting solution is between 50 and 300 centipoise (cps),
preferably between 100 and 200 cps, and is controlled by controlling the molecular weight of the
polymer, the percentage of polymer dissolved in the solvent (between 7% and 18%, depending
5 on the polymer used) and the casting solution temperature (between 0°C and 70°C, preferably
between 15°C and 40°C). To allow for complete penetration of the casting solution into the
support fabric, the casting solution is applied at a rate between 3 and 30 fpm, preferably between
3 and 8 fpm, and with an air quench time between 5 and 60 seconds, preferably between 20 and
10 30 seconds. The advantage of homogenous membranes is that they are very resistant to back
flushing due to the encapsulated design. They are more difficult to manufacture, due to the fact
that an external support mechanism must be designed into the casting machine (FIG. 5) to
support the penetrated support substrate and transport the membrane to the quench tank. This
can be accomplished by rotating a casting drum 83 or supporting the membrane on a continuous
and porous conveyor. This is required because the penetrating casting solution will not allow the
15 membrane to be pulled over a stationary drum prior to quenching.

An asymmetric membrane is formed by coating a polymeric casting solution onto a
support substrate, whereby the porosity of the support and the penetration of the casting solution
allows the casting solution to penetrate the surface of the support fabric but does not allow the
casting solution to penetrate or bleed through the back of the support substrate. The coated
20 membrane film is then allowed an amount of time to form a skin, and then is quenched in a fluid
bath, preferably water, which allows the remainder of the solvent to be removed from the
membrane layer sheet. Because of the chemistry of the casting solution, and the formation of the
membrane skin, the finished membrane has a very dense surface layer with very small and
uniform pores, while the inner layer that supports the surface membrane is much more porous
25 or spongy. Due to the inner layer's high porosity, there is very little resistance to fluid flow, and
only a minimum amount of pressure drop is created for flow of permeate through the membrane,
making the asymmetric design preferable over the homogeneous design. Upon examination of
this membrane layer sheet under a scanning electron microscope (SEM), it can be seen that the
pore size at the membrane surface is very small and uniform, while the polymeric membrane
30 underneath this thin surface layer has very large pores that resemble a spongy material. This lack
of symmetry, or asymmetry, is where these membranes derive their name of asymmetric
membranes. The porosity of the support substrate is between 1 and 10 cfm/ft², preferably
between 1.5 and 3 cfm/ft², with a thickness between 0.002" and 0.008", preferably between
0.003" and 0.005", and a weight between 20 and 100 gm/yd², preferably between 70 and 90
35 gm/yd². The chemistry and physical properties of the casting solution are also important. The
viscosity of the casting solution is between 100 and 1000 centipoise (cps), preferably between
250 and 350 cps, and is controlled by controlling the molecular weight of the polymer, the
percentage of polymer dissolved in the solvent (15%-25% depending on the polymer used), and

1 the casting solution temperature (between 0°C and 70°C, preferably between 15°C and 40°C).
To allow for some penetration of the casting solution into the support fabric, but to prevent bleed
through, the casting solution is applied at a rate of between 5 and 50 fpm, preferably between 5
5 and 10 fpm, and with an air quench time between 5 and 60 seconds, preferably between 20 and
30 seconds. For most traditional applications, the asymmetric membranes are produced to have
very uniform surface pores and adhesion of the membrane to the support substrate is of
secondary concern. In the present invention the adhesion is created through the selection of
polymers, both the fabric and the membrane, that create good chemical bonding, and allowing
10 penetration of the polymer into the fabric support matrix to create additional mechanical
interlocks to further aid in preventing delamination during the backflush cycle.

The process shown in FIG. 5 will now be described. A roll of substrate 82 is unwound
and treated with polymeric casting solution 81. The thickness of the membrane film is controlled
through the use of a mechanical device, either a doctor blade or a precision slot coater, through
which the polymer-solvent casting solution 81 is applied as shown in FIG. 5. To effect a
15 sufficient bond, it is preferable to allow between 5 and 60 seconds of air quench time (air contact
of solution 81 while on the support substrate) prior to immersion in a quench bath 80.
Preferably, the air quench time is between 20 and 30 seconds. The polymer-solvent-support
substrate matrix is first quenched in air to allow the formation of a thin skin, and then quenched
in a suitable fluid 80, preferably water, to allow removal of solvent in solution 81, thus producing
20 a permeable membrane film. Once the solvent has been extracted from the membrane film, the
membrane film may be further treated through heat or additional rinsing, drying, or additional
coating, to obtain the final desired filtration properties. In the case of composite membranes, a
secondary coating may also be applied on top to the membrane film to achieve nanofiltration or
reverse osmosis type membranes.

25 Preferably, the capability of back-flushing is accomplished using a membrane film made
from polymers such as polyethylene, polypropylene, or polysulfone. However, membrane films
which may be employed include polyamides, polyphenylene esters, polyethersulfone,
polysulfonamides, polyvinylidene fluoride, cellulose acetate, cellulose, polyacrylonitrile, or other
film forming polymers.

30 Preferably, the support substrate 76 comprises a non-woven fabric. The support substrate
characteristics vary depending on how whether the membrane film is cast on top of the support
substrate or encased within the polymer matrix. For homogenous membrane filter layer sheets,
a support substrate with a thickness of 0.001"-0.005", but preferably 0.002"-0.004" thick, has a
Frazier air permeability of 1 to 10 cubic feet per minute per square foot (cfm/ft²), preferably 1.5
35 to 3.0 cfm/ft², and a weight from 20-100 grams per square yard (gm/yd)². For asymmetric
membrane filter layer sheets, a support substrate with a thickness of 0.002"-0.008", but
preferably 0.003"-0.005" thick, has a Frazier air permeability of 1.0 to 10.0 cfm/ft², preferably
1.5 to 3.0 cfm/ft², and a weight from 20-100 gm/yd².

1 To further improve the penetration of the casting solution into the support substrate 76,
the casting solution is applied at an elevated temperature in the range of 0°C to 70°C, but
preferably between 15°C and 40°C. For proper adhesion of membrane film 75 to support
substrate 76, the viscosity of the casting solution must be in the range of 100 to 1000 centipoise
5 (cps), but preferably between 250-350 cps.

Several improved chemical, mechanical, and process conditions have been developed to
achieve good mechanical and chemical bonding between membrane film 75 and support
substrate 76. The high back pressures in back-flushing are essential to allow sufficient back flow
of fluids to enable and assure membrane cleaning effectiveness. A combination of membrane
10 polymer casting solution conditions and support substrate 76 properties result in a strongly
bonded composite, sufficient to resist delamination under such high back pressures. Typically,
ultrafiltration membranes have an air quench time of 1-2 seconds to minimize bleed through of
the casting solution through the support substrate. In the present invention, the air quench time
is between 5 and 60 seconds, but preferably between 20 and 30 seconds. If the time is too long,
15 membrane film 75 will bleed through. The combination of a porous support substrate 76 that is
not too highly calendered, a heated and relatively low viscosity casting solution, and an increased
air quench time, creates an ultrafiltration membrane film 75 with sufficient mechanical and
chemical bonding to the support substrate 76 to allow thousands of back-flush cycles at up to 100
psi without adversely affecting the membrane film transport properties. In the present invention,
20 membrane filter layer sheet 71 is capable of withstanding back pressures of up to 100 psi without
delamination of membrane film 75 from support substrate 76, while maintaining the adhesive
seal, and with no other adverse affects on membrane filter layer sheet 71 or element 15
performance properties.

A second preferred embodiment of the present invention is shown in FIG. 6. A spiral
element back-flush system 1¹ has a feed tank 2¹, an air pump 46, an element 15¹, a vacuum
system 52 and a compressed gas tank 49. Element 15¹ is preferably mounted in a vertical
position. Feed tank 2¹ contains a feed solution 100¹ that is kept well mixed via a mechanical
stirrer 3¹. The driving pressure to force feed solution 100¹ into element 15¹ is via vacuum system
52. Air pump 46 is used to promote turbulence at the surface of membrane filter layer sheets 71.
25 Tank 49 uses compressed gas to back flush element 15¹.

Pump 46 compresses gas, preferably air, through a feed pipe 55, a feed pressure control
valve 44 and, eventually, into bubbler 51. A pressure gauge 45 along pipe 55 is used to measure
the pressure from pump 46. Bubbler 51 creates a uniform distribution of fine bubbles 43 which
are directed via a collector 42 into the bottom of membrane filter element 15. Bubbles 43 act as
30 turbulence promoters at the surface of membrane filter layer sheet 71 (see FIG. 6) and help
reduce the boundary layer thickness at the surface of membrane filter layer sheet 71. Bubbles 43
also create a convective flow of feed solution 100 from the bottom through the top of element
15¹, and back to the bottom again.

1 During normal operation, vacuum 52 is applied to permeate collection tube 56 through
a first permeate diverter valve 53 and via a permeate pipe 54 to element 15¹. Permeate pipe 54
preferably includes a permeate accumulator 50. Vacuum system 52 creates a driving pressure
across membrane filter layer sheet 71 resulting in production of a permeate 101¹. Vacuum system
5 52 can be created by a vacuum pump, the suction side of a centrifugal pump, or an aspirator. The
vacuum is preferably in the range of 5 to 29 mm Hg.

In this embodiment, the portion of feed solution 100¹ that permeates element 15¹ is
permeate 101¹. Permeate 101¹ passes through permeate accumulator 50, a first permeate diverter
valve 53, and then, through vacuum system 52. Concentrate 102¹ is defined as the portion of
10 feed solution 100¹ that does not pass through membrane filter element 15¹ and remains in feed
tank 2¹ to be recycled back through filter 15¹.

As shown in FIG. 6, the back-flush fluid is a combination of nitrogen gas from tank 49
and permeate 101¹. The back-flush fluid may be air, nitrogen, or some other suitable gas, alone
or in combination with the permeate fluid. System 1¹ can also be designed to utilize only the
permeate in the back-flush step. This preferred embodiment has the benefits of not requiring a
15 pressure tube for element 15¹, uses an air pump to circulate feed solution 100¹ instead of a pump,
and may result in lower membrane fouling due to the low feed pressure and the turbulence
created by air bubbles 43.

During the back-flush cycle, the permeate diverter valve 53 is activated allowing the
back-flush fluid to enter permeate collection tube 56. Nitrogen, from compressed gas tank 49,
is fed through a pressure regulator 47. After passing through pressure regulator 47, nitrogen
moves through a gas pipe 48, permeate diverter valve 53, and into the permeate pipe 54.
20 Preferably, the initial back-flush fluid would be permeate 101¹ stored in accumulator 50,
followed by the nitrogen gas. The use of nitrogen gas as back flush fluid results in increased
turbulence on the surface of membrane filter layer sheet 71, further aiding in the removal of
foulants. After a set period of time, permeate diverter valve 53 is again activated and system 1¹
returns to normal operation. This process of creating permeate 101¹ through vacuum system 52
and periodic back-flushing is repeated on a regular basis to maintain a steady state flux rate
through membrane filter element 15¹.

30 The following examples serve to further illustrate the invention, but should not be
construed as in any way limiting the broader aspects thereof.

EXAMPLE 1

35 An ultrafiltration membrane film was cast on a support substrate that was porous enough
to allow good penetration of the casting solution into the support substrate structure to insure a
good mechanical bond, but not too porous as to allow excessive bleed through of the casting
solution. The substrate polymer also had to have good chemical affinity for the membrane casting
solution. Although there may be other substrates that could perform this function, we obtained

1 excellent results with a dry lay polyester non-woven substrate, with a weight of 80 grams per
square yard, 0.004" thick, and a Frazier air permeability of 1.5 to 3 cubic feet per minute per
square foot (cfm/ft²). The Frazier air permeability is a measure of the porosity of the substrate.
5 These substrates are produced using short polyester fibers that are "carded" into felts that are
relatively thick, and then are "calendered" between a steel and felt roll under high pressure and
temperature to obtain the proper porosity, thickness, and weight. Many substrates used in these
applications are highly "calendered" resulting in a support substrate having a paper-like finish.
While this type of a finish gives a uniform coating surface with few defects and small pores, the
dense, paper like finish makes it difficult for the casting solution to penetrate, and as a result, the
10 membrane film is easily delaminated.

In this example, we cast an ultrafiltration membrane film using a 18% BASF
polyethersulfone polymer dissolved in 23% DMF and 55% NMP, to give a mixed viscosity of
320 centipoise. This formulation gave good penetration and adhesion to the support substrate,
and was coated at a thickness of 0.0028".

15 To further improve the penetration of the casting solution into the support substrate, the
casting solution was applied at an elevated temperature of 30°C. The casting solution was then
allowed an air quench time of 26 seconds prior to immersion in the solvent extraction bath which
was chilled to 10°C. The membrane filter layer sheet was cast at 8 feet per minute (fpm). The
membrane filter layer sheet was then fed into a heat treat tank filled with 65°C water to anneal
and heat set the membrane filter layer sheet. The membrane filter layer sheet was tested under
20 30 psi of pressure with 500 ppm of a 76,000 MW dextran solution. The membrane filter layer
sheet exhibited a flux of 30 GFD at 97 % rejection.

This membrane filter layer sheet was then wound into two spiral elements with a 2.5"
diameter and a length of 14" long using the custom formulated adhesive.

25 The element was then placed in a FRP pressure tube tested with a solution of DI water and
a mixture of hexamethylene tetramine and hydrazine sulfate. This mixture forms uniform and
well distributed suspended particles in the 1-5 micron range and is used as a standard for
turbidity measurements. The feed turbidity was maintained between 50 and 100 NTU. This feed
solution was pressurized with a feed pump to 30 psi and fed to the two 2514 elements. The
30 elements exhibited a combined permeate flow of 1.2 liters per minute and produced a permeate
turbidity of 0.1 NTU's. The permeate turbidity was used as an indicator of membrane integrity.
If the membrane integrity was compromised during the back-flush cycles, the permeate turbidity
would increase. The element was then run on standard tap water at 30 psi during the feed. Every
30 seconds, the element was back-flushed with nitrogen at 15 psi for 15 seconds. This cycle was
35 repeated for 2030 cycles. The element was then retested with the hexamethylene tetramine and
hydrazine sulfate turbidity standard and exhibited a combined permeate flow of 1.1 lpm and a
permeate turbidity of 0.1 NTU's. This test indicates that the membrane filter layer sheet and
element maintained their integrity during this test and did not delaminate.

EXAMPLE 2

A microfiltration membrane film was cast on a support substrate as in Example 1. However, in this example, a BASF polyvinylidene fluoride polymer was dissolved in 80% DMF, to give a mixed viscosity of 350 centipoise. This formulation gave good penetration and adhesion to the support substrate.

To further improve the penetration of the casting solution into the support substrate, the casting solution was applied at an elevated temperature of 30°C. The casting solution was then allowed an air quench time of 20 seconds prior to immersion in the solvent extraction bath. The membrane filter layer sheet was tested under 10 psi of pressure with 500 ppm of hexamethylene tetramine and hydrazine sulfate turbidity standard. The membrane filter layer sheet exhibited a flux of 35 GFD at 10 psi and the permeate produced had a turbidity of <0.1 NTU.

This membrane filter layer sheet was then wound into two spiral elements with a 2.5" diameter and a length of 14" long using the E.V. Roberts 1752 adhesive. The element was then placed in a FRP pressure tube tested with a solution of hexamethylene tetramine and hydrazine sulfate turbidity standard at 30 psi. The element exhibited a flux of 35 GFD and a permeate turbidity of 0.2 NTU. The element was then run on standard tap water at 10 psi in a back-flush cycle. Every 30 seconds, the element was back-flushed with nitrogen at 30 psi for 15 seconds. This cycle was repeated for 1236 cycles. The element was then retested with the hexamethylene tetramine and hydrazine sulfate turbidity standard at 10 psi and exhibited 34 GFD and a permeate turbidity of <0.1 NTU. This example indicates that the membrane filter layer sheet and element maintained their integrity during this test and did not delaminate.

EXAMPLE 3

The test of Example 1 was repeated using the same element but with an increased back-flush pressure of 30 psi. The element was then placed in a FRP pressure tube tested with a solution of DI water and a mixture of hexamethylene tetramine and hydrazine sulfate. The feed turbidity was maintained between 50 and 100 NTU. The elements exhibited a combined permeate flow of 1.4 liters per minute and produced a permeate turbidity of 0.1 NTU's. This cycle was repeated for 1400 cycles. The element was then retested with the hexamethylene tetramine and hydrazine sulfate turbidity standard and exhibited a combined permeate flow of 1.5 lpm and a permeate turbidity of 0.2 NTU's. This test indicates that the membrane filter layer sheet and element maintained their integrity during this test and did not delaminate.

EXAMPLE 4

The test of Example 1 was repeated using the same element but with an increased back-flush pressure of 45 psi. The element was then placed in a FRP pressure tube tested with a solution of DI water and a mixture of hexamethylene tetramine and hydrazine sulfate. The feed

1 turbidity was maintained between 50 and 100 NTU. The elements exhibited a combined
permeate flow of 1.7 liters per minute and produced a permeate turbidity of 0.5 NTU's. This
cycle was repeated for 1000 cycles. The element was then retested with the hexamethylene
5 tetramine and hydrazine sulfate turbidity standard and exhibited a combined permeate flow of
1.6 lpm and a permeate turbidity of 0.15 NTU's. This test indicates that the membrane filter layer
sheet and element maintained their integrity during this test and did not delaminate.

EXAMPLE 5

10 The test of Example 1 was repeated using the same element but with an increased back-
flush pressure of 60 psi. The element was then placed in a FRP pressure tube tested with a
solution of DI water and a mixture of hexamethylene tetramine and hydrazine sulfate. The feed
turbidity was maintained between 50 and 100 NTU. The elements exhibited a combined
permeate flow of 1.6 liters per minute and produced a permeate turbidity of 0.1 NTU's. This
cycle was repeated for 620 cycles. The element was then retested with the hexamethylene
15 tetramine and hydrazine sulfate turbidity standard and exhibited a combined permeate flow of
1.6 lpm and a permeate turbidity of 0.10 NTU's. This test indicates that the membrane filter layer
sheet and element maintained their integrity during this test and did not delaminate.

20 At the conclusion of the test, three small pinholes were punctured into one of the
membrane filter elements to determine the sensitivity of the turbidity test. The element was
retested with a solution of DI water and a mixture of hexamethylene tetramine and hydrazine
sulfate with a feed turbidity of 55 NTU's and the permeate turbidity was 7.7 NTU's. This
indicates that the turbidity test is a sensitive indicator of element integrity.

EXAMPLE 6

25 A 4" diameter by 40" long element was produced using the preferred membrane filter
layer sheet and the preferred adhesive as in Example 1. The element was placed in a well stirred
tank containing a mixture of 0.5% diatomaceous earth and 500 ppm dextran with a molecular
weight of between 5-20 million daltons as a synthetic fouling solution, which had a turbidity
above 100 NTU. The permeate collection tube was connected to a vacuum system that
30 maintained a vacuum of 16 inches of mercury (in Hg) to provide the driving pressure for
permeation of the feed solution through the membrane filter layer sheet. The element exhibited
an initial flux of 13 GFD and the permeate turbidity was <0.1 NTU, indicating good mechanical
integrity. Under the element, as shown in FIG. 6, air bubbles were produced using a porous
sintered metal plate. Air was supplied using a low pressure air blower operating at a pressure of
35 2 inches of water (in H₂O) to circulate the feed solution across the surface of the membrane filter
layer sheet and promote turbulence to minimize the boundary layer thickness. The element was
operated for 30 minutes and then back-flushed with permeate for 5 seconds followed by air for
15 seconds. This operation was repeated for 14 days of operation. The element exhibited a flux

1 of 12 GFD after the 14 days of operation. The turbidity of the permeate was <0.1 NTU indicating
that the element integrity had not been compromised. The same element was then operated under
the same conditions but without the back-flush cycle. After 5 days of operation, the flux had
declined to 4 GFD. This example indicates that the back-flush cycle is beneficial in removing
5 foulants from the surface of the membrane filter layer sheet.

EXAMPLE 7

A 4" diameter by 40" long element was produced using the preferred membrane filter
layer sheet and adhesive as in Example 1. The element was placed into a vertically mounted
10 pressure tube with the feed solution entering the bottom of the pressure tube and the concentrate
being removed from the top of the pressure tube as shown in FIG. 1. The element exhibited an
initial flux of 8 GFD and the permeate turbidity was <0.1 NTU, indicating good mechanical
integrity. The feed was pressurized to 15 psi during the trial. The element is operated in this
mode for 30 minutes and is then back-flushed with permeate for 5 seconds followed by a back-
flush of 15 seconds with nitrogen. During the back-flush the three-way valves are activated
allowing the foulants that are back-flushed from the element to exit from the bottom of the
pressure tube and also allowing the feed solution to enter the top of the pressure tube. This
reverse feed flow allows gravity to help in removing foulants and suspended solids from the
element and pressure tube during back-flush cycle. This operation was repeated for 14 days of
operation. The element exhibited a flux of 7 GFD after the 14 days of operation. The turbidity
of the permeate was <0.1 NTU indicating that the element integrity had not been compromised.
The same element was then operated under the same conditions but without the back-flush cycle.
After 4 days of operation, the flux had declined to 3 GFD. This example indicates that the back-
flush cycle is beneficial in removing foulants from the surface of the membrane filter layer sheet.

The preceding description indicates the preferred embodiments of the present invention,
but it is not limited to the designs shown. Therefore, the present invention is not intended to be
limited to the working embodiments described above. Thus, it will be understood that within the
scope of the following claims, this invention may be practiced otherwise than as specifically
described.

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1 CLAIMS:

1. A spiral wound membrane filtration element capable of being back-flushed comprising:
 a permeate carrier sheet,
 5 a membrane filter layer sheet adhesively bonded to the permeate carrier sheet, and having a support substrate, and a membrane film over the support substrate; and
 a feed spacer sheet in between layers of membrane filter layer sheets;
 wherein the support substrate has a Frazier air permeability between 0.1 and 10 cfm/ft;
 wherein the membrane filter layer sheet is adhesively bonded to the permeate carrier with
 10 adhesive capable of retaining the bond during element back-flushing.
 wherein the feed spacer sheet, the membrane filter layer sheets, and the permeate carrier sheet are wrapped around a permeate collection tube.
- 15 2. The element of claim 1 wherein the feed spacer sheet has a thickness between 0.02" and 0.10."
3. The element of claim 2 wherein the feed spacer sheet has a thickness between 0.04" and 0.06."
- 20 4. The element of claim 1 wherein fluid is capable of flowing through the support substrate and the membrane film does not delaminate from the substrate during the back-flushing cycle.
- 25 5. The element of claim 1 wherein the membrane filtration element utilizes a micro-filtration process.
6. The element of claim 1 wherein the membrane filtration element utilizes an ultrafiltration process.
- 30 7. The element of claim 1 wherein the membrane filtration element utilizes a nanofiltration process.
8. The element of claim 1 wherein the membrane filtration element utilizes a reverse osmosis process.
- 35 9. The element of claim 1 wherein there are multiple layers of the membrane filter layer sheets, feed spacer sheets, and permeate carrier sheets wrapped around the permeate collection tube.

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10. The element of claim 1 wherein the membrane filter layer sheet is adhesively bonded to the permeate carrier sheet with adhesive having an overlap shear strength of at least 300 psi.

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11. The element of claim 10 wherein the adhesive is manufactured by E.V. Roberts of Culver City, California, model number 1752.

10

12. A method of making a back-flushable spiral wound membrane filtration element having a filter layer and a permeate collection tube, the method comprises:
forming a membrane filter layer sheet with a support substrate having a Frazier air permeability between 0.1 and 10 cfm/ft²;

15

cutting the membrane filter layer sheet to a desired length;
placing a cut piece of a feed spacer sheet on top of the membrane filter layer sheet, the width of the feed spacer sheet being approximately half the width of the membrane filter layer sheet;

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folding the membrane filter layer sheet over the feed spacer so that the feed spacer sheet is sandwiched between two layers of the membrane filter layer sheet;
attaching a center side part of a permeate carrier sheet to the permeate collection tube;
applying an adhesive seal on the permeate carrier sheet along sides other than the center side part;

25

positioning the membrane filter layer sheet-feed spacer sheet sandwich over the permeate carrier sheet such that the adhesive seal bonds the membrane filter layer sheet to the permeate carrier sheet; and
wrapping the permeate carrier sheet, the membrane filter layer sheet, and the feed spacer sheet around the permeate collection tube.

30

13. The method of claim 12 further comprising preventing feed solution from entering the permeate collection tube.

35

14. The method of claim 12 wherein the back-flush, pressure-resistant adhesive is manufactured by E.V. Roberts of Culver City, California, model number 1752.

35

15. A membrane filter layer sheet for a spiral wound membrane filtration element capable of being back flushed, the filter sheet comprising:
a support substrate; and
a membrane film over the support substrate;
wherein the support substrate has a Frazier air permeability between 0.1 and 10 cfm/ft².

INTENDED SHEET

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- 1 16. The membrane filter layer sheet of claim 15 wherein the support substrate comprises a non-woven fabric.
- 5 17. The membrane filter layer sheet of claim 15 wherein the membrane film is cast on top of the support substrate to form an asymmetric membrane filter layer sheet.
18. The membrane filter layer sheet of claim 17 wherein the support substrate has a thickness between 0.002" and 0.008."
- 10 19. The membrane filter layer sheet of claim 18 wherein the support substrate has a thickness between 0.003" and 0.005".
20. The membrane filter layer sheet of claim 17 wherein the support substrate has a Frazier air permeability between 1.5 and 3.0 cfm/ft².
- 15 21. The membrane filter layer sheet of claim 17 wherein the support substrate has a weight between 20 and 100 gm/yd².
- 20 22. The membrane filter layer sheet of claim 15 wherein the membrane film comprises a polymeric material.
23. The membrane filter layer sheet of claim 15 wherein the membrane film is encased around the support substrate to form a homogenous membrane filter layer sheet.
- 25 24. The membrane filter layer sheet of claim 23 wherein the support substrate has a thickness between 0.001" and 0.005".
25. The membrane filter layer sheet of claim 24 wherein the support substrate has a thickness between 0.002" and 0.004".
- 30 26. The membrane filter layer sheet of claim 23 wherein the support substrate has a Frazier air permeability between 0.5 and 1.0 cubic feet per minute per square foot.
27. The membrane filter layer sheet of claim 23 wherein the support substrate has a weight between 20 and 100 grams per square yard.
- 35 28. A method of creating a permeable back flushable membrane filter layer sheet comprising:

1 placing a casting solution of a certain thickness on a passing support substrate with a
Frazier air permeability between 0.1 and 10 cfm/ft²;

controlling the thickness of the casting solution on the support substrate through use of
a mechanical device for dispensing the casting solution; and

5 immersing the substrate with the casting solution into a quench bath to allow removal of
casting solution after an air quench time that allows formation of a thin skin on the support
substrate.

29. The method of claim 28 wherein the mechanical device is one of a doctor blade and
10 a precision slot coater.

30. The method of claim 28 wherein the quench bath is water.

31. The method of claim 28 further comprising treating the permeable membrane filter
15 layer with one of heat, additional rinsing, drying, and additional coating.

32. The method of claim 28 wherein the casting solution is polymeric.

33. The method of claim 32 wherein the solvent into which the polymer is dissolved
20 is one of dimethylformamide, 1,4 dioxane, acetone, and n-methyl pyrrolidone.

34. The method of claim 33 wherein the polymers are one of polyethylene,
polypropylene, polysulfone, polyamides, polyphenylene esters, polyethersulfone,
polysulfonamides, polyvinylidene fluoride, cellulose acetate, cellulose, polyacrylonitrile,
25 and other film forming polymers.

35. The method of claim 28 wherein the casting solution is heated.

36. The method of claim 35 wherein the casting solution is applied at an elevated
30 temperature in the range of 0°C to 70°C.

37. The method of claim 36 wherein the casting solution is applied at an elevated
temperature in the range of 15°C to 40°C.

38. The method of claim 28 wherein the viscosity of the casting solution is between
35 100 and 1000 centipoise.

39. The method of claim 38 wherein the viscosity of the casting solution is between

- 1 250 and 350 centipoise.
40. The method of claim 28 wherein the membrane filter layer sheet is homogenous.
- 5 41. The method of claim 28 wherein the membrane filter layer sheet is asymmetric.
42. The method of claim 28 wherein the air quench time has a duration between 5 and 60 seconds.
- 10 43. The method of claim 42 wherein the air quench time has a duration between 20 and 30 seconds.
44. A spiral wound membrane filtration element capable of being back-flushed comprising:
 a permeate carrier sheet;
 a membrane filter layer sheet adhesively bonded to the permeate carrier sheet with model number 1752 adhesive manufactured by E.V. Roberts of Culver City, California, the membrane filter layer sheet having a support substrate, and a membrane film over the support substrate; and
 a feed spacer sheet in between layers of membrane filter layer sheets;
 wherein the feed spacer sheet, the membrane filter layer sheets, and the permeate carrier sheet are wrapped around a permeate collection tube.
- 15 45. A back-flush system for a back-flushable spiral wound membrane filtration element comprising:
 feed solution for the filtration element from a source;
 a feed pump for pumping and pressurizing the feed solution from the source through the filtration element;
 a feed pipe through which the pressurized feed solution flows to the element;
 an element pressure tube wherein a first portion of the feed solution permeates the
30 membrane filtration element as a permeate, and a second portion of the feed solution does not permeate and exits the membrane filtration element as a concentrate;
 a feed diverter valve for controlling flow from the feed pipe to the pressure tube;
 a source of compressed gas capable of back-flushing the membrane filtration element; and
 a concentrate diverter valve for controlling the flow rate of concentrate out of the exiting
35 pressure tube.
46. A method of cleaning the spiral wound membrane filtration element comprising:
 applying pressurized feed solution having solids to an outer surface of a membrane filter

1 layer sheet in the element;

passing a portion of feed solution through the membrane filter layer sheet as a permeate;
retaining a portion of the feed solution solids in pores of the membrane filter layer sheet;
removing the non-retained solids from the element with the remainder of the feed solution;

5 allowing the permeate to flow in a first direction through a permeate collection tube of the
element; and

introducing a pressurized back flush fluid with a pressure that exceeds the feed pressure,
on a periodic basis, into the permeate collection tube in a second direction opposite the first
direction to dislodge a substantial portion of the retained solids on the pores of the membrane
10 filter layer sheet.

47. The method of claim 46 further comprising:

pumping the feed solution from the source using a feed pump;

pressurizing the feed solution in the pump;

pumping the pressurized feed solution through the filtration element using the feed pump;

controlling flow from a feed pipe to the element using a feed diverter valve;

controlling the flow rate of concentrate out of the exiting the element using a concentrate
diverter valve;

controlling the flow rate of concentrate out of the concentrate diverter valve using a
concentrate valve;

holding permeate for the back-flush step using a permeate accumulator; and

controlling the flow of permeate out of the permeate accumulator and the flow rate of the
backflush gas while back-flushing using a permeate diverter valve.

48. The method of claim 46 wherein the pressure on the back-flush gas is controlled
by a gas regulator; and the back-flush pressure is greater than the feed pressure on the
element by between 10 and 30 psi.

49. The method of claim 46 wherein the pressure from the back flush fluid on the
element is between 5 and 100 psi.

50. The method of claim 49 wherein the pressure from the back flush fluid on the
element is between 20 and 60 psi.

51. The method of claim 46 wherein the back flush fluid comprises at least one of
compressed gas, air, nitrogen, permeate, and cleaning solution.

52. The method of claim 46 wherein the back flush fluid comprises permeate followed

1 by compressed air.

53. A back-flush system for a spiral wound membrane element comprising:

a feed tank having feed solution;

5 a permeate collection tube placed in the feed tank, wherein the permeate collection tube includes a spiral wound membrane element having a permeate carrier sheet, a feed spacer sheet, and a membrane filter layer sheet with a supporting substrate and a membrane film superimposed on the supporting substrate;

10 a bubbler having bubbles acting as turbulence promoters at the surface of the membrane filter layer sheet for reducing the boundary layer thickness at the surface of the membrane filter layer sheet, and creating a convective flow of feed solution from the bottom through the top of the element, and returning back to the bottom;

a source of pressurized back flush fluid used in forcing permeate from a permeate accumulator and back flush fluid back to the element; and

15 a vacuum system having a vacuum for creating the driving pressure to force the feed solution into the element thereby creating permeate.

54. The back-flush system of claim 53 further comprising:

an air pump for compressing gas for the bubbler; and

20 a permeate diverter valve, wherein the permeate diverter valve is capable of controlling permeate flow and reversing the permeate flow to back-flush any foulants from the surface of the membrane filter layer sheet.

55. The back-flush system of claim 54 further comprising a cycle of back flushing;

25 wherein the duration of the back flush cycle is 5 to 30 seconds;

wherein in between back flush cycles, the permeate diverter valve is activated to return the system to extracting permeate from the feed solution.

56. The back-flush system of claim 53 wherein the back flush fluid comprises at least 30 one of compressed gas, air, nitrogen, permeate, and cleaning solution.

57. The back-flush system of claim 53 wherein the back flush fluid comprises permeate followed by compressed air.

58. The back-flush system of claim 53 wherein the vacuum is in the range of 5 to 29 35 mm Hg.

59. A method of back-flushing the spiral wound membrane element through a back-

1 flush system comprising:
placing a spiral wound membrane element into a feed tank;
promoting turbulence at a surface of the membrane filter layer sheet through a bubbler
having bubbles which are capable of:

5 reducing a boundary layer thickness at the surface of the membrane filter layer
sheet;

creating a convective flow of pressurized feed solution from a bottom through a top
of the element; and

10 returning the feed solution back to the bottom of the element; and
introducing on a periodic basis a pressurized back flush fluid, with a pressure that exceeds
the feed pressure, into the element in a direction from top to bottom of the element to dislodge
a substantial portion of feed solution solids retained on pores of the membrane filter layer sheet.

60. The method of claim 59 further comprising:

compressing gas for the bubbler using an air pump;

creating the driving pressure to force the feed solution into the element thereby creating
permeate using a vacuum system having a vacuum;

directing the flow rate of permeate out of the permeate accumulator and the flow rate of
gas out of the tank while back-flushing using a permeate diverter valve;

20 activating a permeate diverter valve allowing back flush fluid to enter the element to back-
flush the feed solution solutions foulants from the surface of the membrane filter layer sheet in
the element.

61. The method of claim 59 wherein the pressure on the back-flush gas is controlled
25 by a gas regulator; and the back-flush pressure is greater than the feed pressure on the
element by between 10 and 30 psi.

62. The method of claim 59 wherein the pressure from the back flush fluid on the
element is between 5 and 100 psi.

30 63. The method of claim 62 wherein the pressure from the back flush fluid on the
element is between 20 and 60 psi.

64. The method of claim 59 wherein the back flush fluid comprises at least one of
35 compressed gas, air, nitrogen, permeate, and cleaning solution.

65. The method of claim 59 wherein the back flush fluid comprises permeate followed
by compressed air.

FIG. 1

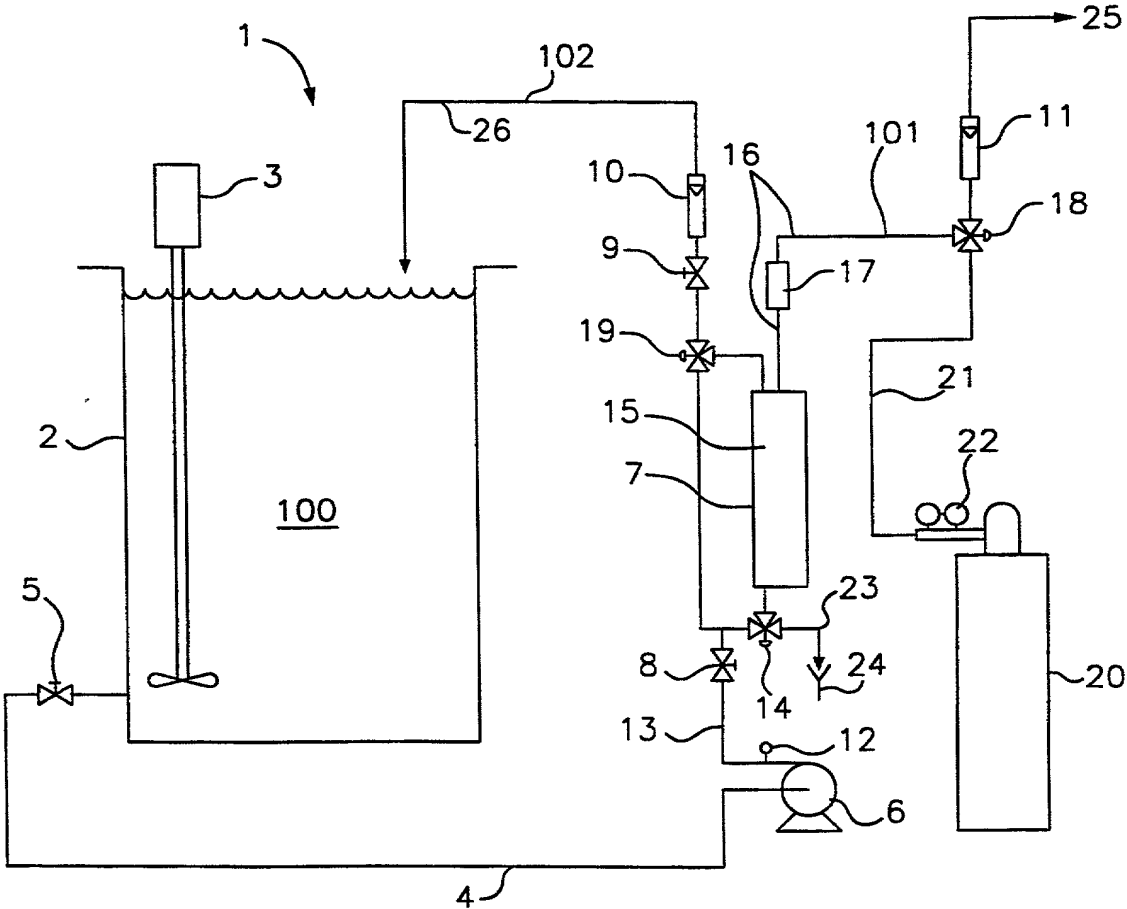


FIG. 2

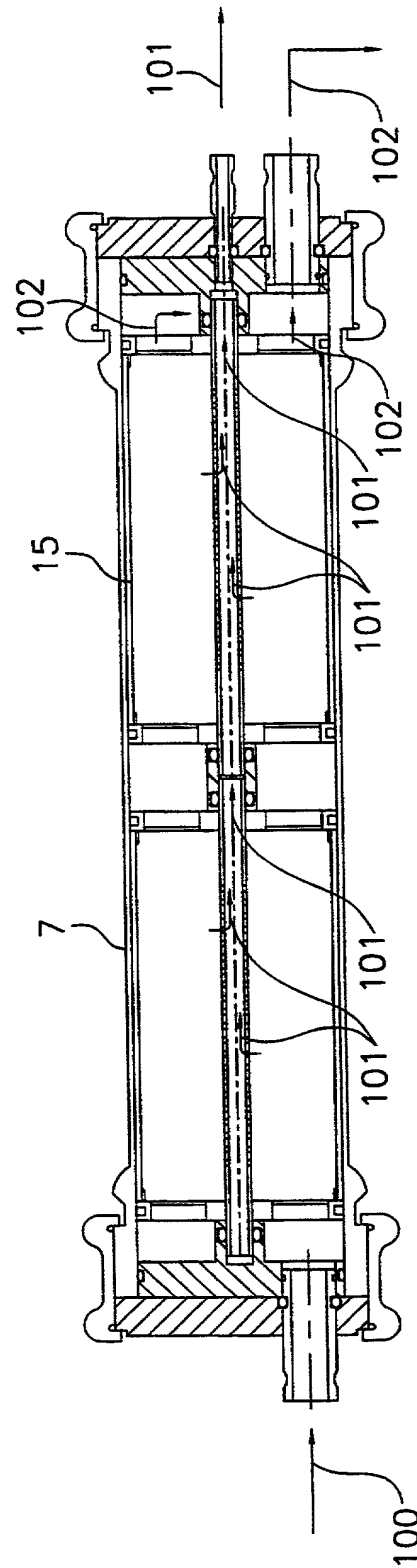
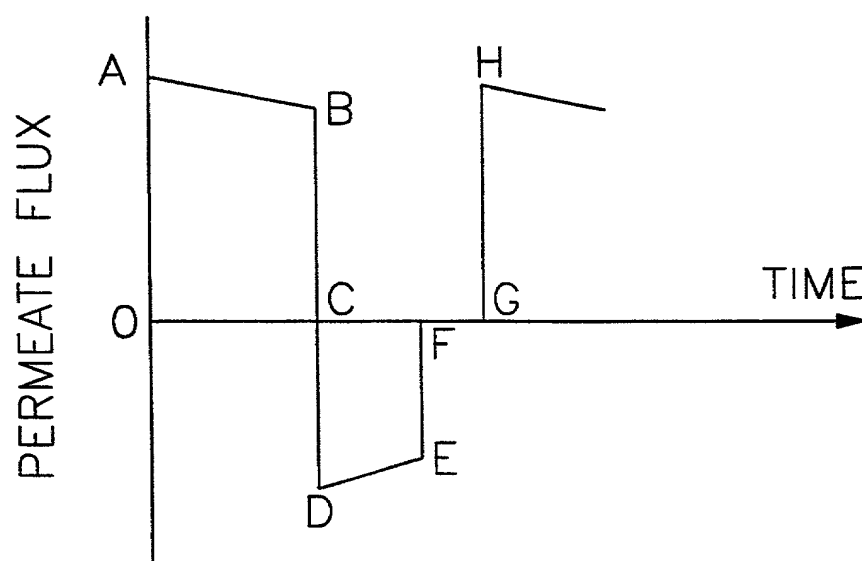


FIG. 3

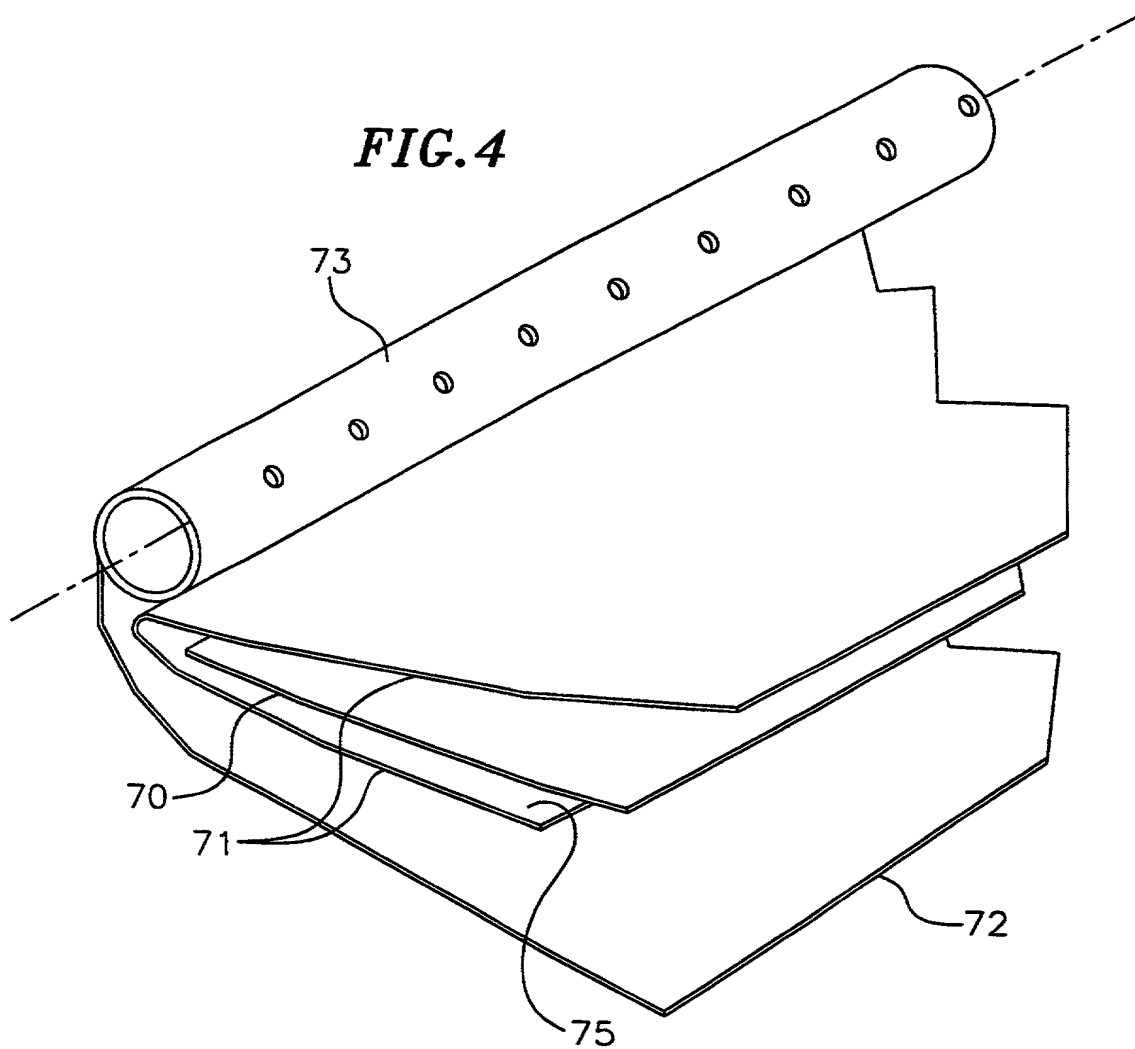
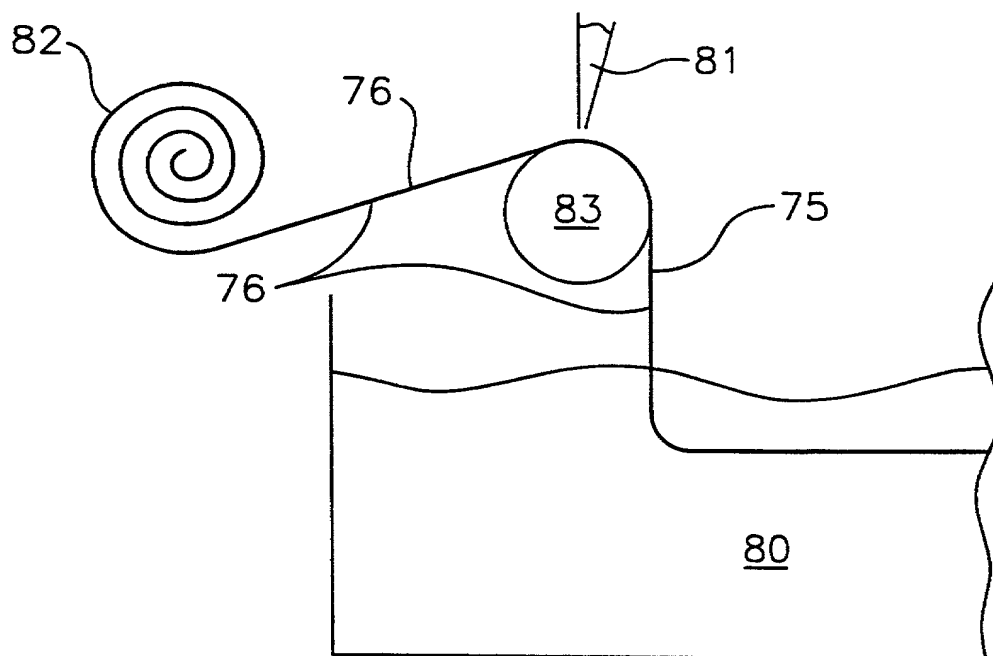


FIG. 5





DECLARATION AND POWER OF ATTORNEY
FOR PATENT APPLICATION

Docket No. : 33683/TJD/T358

As a below named inventor, I hereby declare that:

My residence, mailing address and citizenship are as stated below next to my name.

I believe I am the original, first and sole inventor (if only one name is listed below) or an original, first and joint inventor (if plural names are listed below) of the subject matter which is claimed and for which a patent is sought on the invention entitled BACK-FLUSHABLE SPIRAL WOUND FILTER AND METHODS OF MAKING AND USING SAME, the specification of which is attached hereto unless the following is checked:

X was filed on June 22, 1999 as United States Application Number or PCT International Application Number PCT/US99/13934 and was amended on (if applicable).

I hereby state that I have reviewed and understand the contents of the above-identified specification, including the claims, as amended by any amendment specifically referred to above.

I acknowledge the duty to disclose information which is material to patentability as defined in 37 CFR § 1.56, including for continuation-in-part applications, material information which became available between the filing date of the prior application and the national or PCT international filing date of the continuation-in-part application.

I hereby claim foreign priority benefits under 35 U.S.C. § 119(a)-(d) or § 365(b) of the foreign application(s) for patent or inventor's certificate, or § 365(a) of any PCT International application which designated at least one country other than the United States of America, listed below and have also identified below, any foreign application for patent or inventor's certificate, or any PCT International application having a filing date before that of the application on which priority is claimed.

Prior Foreign Application(s)

<u>Application Number</u>	<u>Country</u>	<u>Filing Date (day/month/year)</u>	<u>Priority Claimed</u>
PCT/US99/13934	PCT	22 June 1999	YES

I hereby claim the benefit under 35 U.S.C. § 119(e) of any United States provisional application(s) listed below.

<u>Application Number</u>	<u>Filing Date</u>
---------------------------	--------------------

I hereby claim the benefit under 35 U.S.C. § 120 of any United States application(s), or any PCT International application designating the United States, listed below and, insofar as the subject matter of each of the claims of this application is not disclosed in the prior United States or PCT International application in the manner provided by the first paragraph of 35 U.S.C. § 112.

<u>Application Number</u>	<u>Filing Date</u>	<u>Patented/Pending/Abandoned</u>
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**DECLARATION AND POWER OF ATTORNEY
FOR PATENT APPLICATION**

Docket No. 33683/TJD/T358

POWER OF ATTORNEY: I hereby appoint the following attorneys and agents of the law firm CHRISTIE, PARKER & HALE, LLP to prosecute this application and any international application under the Patent Cooperation Treaty based on it and to transact all business in the U.S. Patent and Trademark Office connected with either of them in accordance with instructions from the assignee of the entire interest in this application; or from the first or sole inventor named below in the event the application is not assigned; or from __ in the event the power granted herein is for an application filed on behalf of a foreign attorney or agent.

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I declare that all statements made herein of my own knowledge are true and that all statements made on information and belief are believed to be true; and further that these statements were made with the knowledge that willful false statements and the like so made are punishable by fine or imprisonment, or both, under 18 U.S.C. 1001 and that such willful false statements may jeopardize the validity of the application or any patent issued thereon.

DECLARATION AND POWER OF ATTORNEY
FOR PATENT APPLICATION

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